Geothermal Reservoir Monitoring Using Multi-geophysical Survey Techniques

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Abstract

Prediction of the behavior of a geothermal reservoir under exploitation conditions is carried out based upon numerical models of the reservoir. Since the uncertainty in the predictions of numerical reservoir models is directly related to the amount of field data available against which the models can be tested, it is clear that the addition of repeat geophysical survey data to the list of pertinent field measurements is likely to improve the reliability of these forecasts.

The application of improved geophysical techniques to reservoir management was among the objectives of a geothermal R&D project which was carried out by NEDO from 1997 through 2002. GSJ has been carrying out supporting basic research in cooperation with NEDO: pursuing the development of improved field survey techniques and associated modeling studies involving various passive and active geophysical survey techniques and their application to reservoir performance monitoring.

In this project, the so-called mathematical postprocessors have been developed to calculate time-dependent earth-surface distributions of geophysical observables such as microgravity, self-potential, and apparent resistivity (from either DC or MT/CSMT surveys). The temporal changes are caused by changing underground conditions (pressure, temperature, salinity, gas saturation, etc.) as computed by numerical unsteady multidimensional thermohydraulic reservoir/aquifer simulations. The postprocessors enable us to incorporate repeat geophysical survey data into "history-matching" studies, which is especially useful for appraising the volumetric properties of any proposed mathematical reservoir model.

























Basic equationsMass conservation
$$\frac{\partial}{\partial t} \left[\phi \sum_{j} (S_{j} \rho_{j} C_{kj}) \right] + \sum_{j} \nabla \cdot \left(\overrightarrow{M}_{j} C_{kj} - L \middle| \overrightarrow{M}_{j} \middle| \nabla C_{kj} \right) = n \&_{in} C_{k}^{in} - n \&_{out} C_{k}^{flow}$$
Energy conservation $\frac{\partial}{\partial t} \left[(1 - \phi) \rho_{R} C_{VR} T + \phi \sum_{j} (S_{j} \rho_{j} E_{j}) \right] + \sum_{j} \nabla \cdot \left(\overrightarrow{M}_{j} H_{j} - L \middle| \overrightarrow{M}_{j} \middle| \nabla H_{j} \right) \right]$ $= \nabla \cdot (\kappa \nabla T) + \sum_{j} \overrightarrow{M}_{j} \cdot \overrightarrow{g} + n \&_{in} H^{in} - n \&_{out} H^{flow} + \&$ Momentum conservation $\overrightarrow{M}_{j} = \frac{KR_{j}}{V_{j}} \left(\rho_{j} \overrightarrow{g} - \nabla P_{j} \right)$

































































































